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S-3A BALLAST BLOCK FINAL DESIGN AND ENGINEERING TESTS

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The S-3A Ballast Block is a 169 pound (77 Kg) assembly of four (4) interlocking aluminum blocks. It is used to control the trajectory of an unoccupied 1E-1 ejection seat.

Tests indicate that it meets all functional and structural requirements for use in the S-3A aircraft.

It provides a simple cost effective replacement for anthropomorphic dummies presently being used as ballast.

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SUMMARY

The third prototype S-3A Ballast Block weighs 169 pounds (77 Kg). It is an assembly of four interlocking aluminum blocks. One crewman can carry two blocks at a time into the aircraft where he can quickly assemble the unit either on the 1E-1 ejection seat or on the avionics aisleway step. Restraint on the ejection seat is obtained by connecting the four quick disconnect adjuster fittings on the ejection seat to fittings on the Ballast Block. When the Assembly is placed on the avionics aisle steps it is restrained with two aluminum locking plates which are bolted to the top block. These plates extend beyond the edges of the block and fit into keyways on either side of the main bulkhead forgings directly behind the aft ejection seats.

When the Block is secured on the 1E1-1 seat the overall center of gravity falls 0.72 inches below the centerline of rocket thrust. The Ballast Block meets all operational and structural requirements for safe function in the aircraft. It can be maintained at the Operational level; the only parts that may need replacement are straps which are readily available.

The S-3A Ballast Block provides a simple and cost effective replacement for anthropomorphic dummies presently being used to ballast unoccupied 1E1 ejection seats.

INTRODUCTION

BACKGROUND

The S-3A aircraft has (4) ejection seats. Both the pilot and copilot have Command Eject Selector levers which allow them the option to eject all crewmembers or "Self Eject." If one of the aft seats is unoccupied, and "Command Eject" is selected, the unoccupied seat will accelerate ahead of the occupied seat next to it. Two hazards exist; first, the crewmember next to the unoccupied seat could be burned by the rocket plume from the empty seat which has a higher acceleration; second, the empty seat could tumble into one of the other seats because the center of gravity and the center of rocket thrust are too far apart. To eliminate these hazards it is necessary to ballast the unoccupied seat. This is presently being done with anthropomorphic test dummies, if they can be obtained. Unfortunately these dummies have various weights and are usually damaged (i.e. arms, legs, or head missing). There is no guarantee that the center of gravity is in the proper location to prevent tumbling. To correct this potentially dangerous situation the Naval Air Systems Command tasked the Naval Air Development Center to design a ballast block. After the initial prototype was developed and tested, references (1) and (2) recommended changes to be incorporated into the final design.

DESCRIPTION OF FINAL DESIGN

The S-3A Ballast Block is an assembly of four (4) interlocking aluminum blocks that can be strapped into an ESCAPAC 1E-1 seat and can also be securely stored in the aisle on the avionics bay step of the S-3A aircraft (figures 1 & 2).

Two blocks at a time can be carried by one man (figure 3). Each block weighs about 42 pounds (19 Kg).

Straps on the top and bottom blocks have quick disconnect fittings that mate with the parachute/inertia reel straps and with the survival kit straps to mount the assembly on the 1E1 ejection seat (figure 11).

Each block has a handle and a finger ledge on two sides that enable the crewmember to assemble the blocks on the seat without danger of pinching fingers (figure 4).

The center of gravity of the block/seat assembly falls less than one inch (three centimeters) below the center of the rocket thrustline (figure 29).

Aluminum is used to make the assembly antimagnetic so as not to interfere with submarine detection systems.

Each block is stenciled with its number to simplify assembly (figure 1).

Two locking plates are bolted to the top block. They are used to lock the assembly in the aisle position for catapult, arrestment, and flight loads (figure 19).

DISCUSSION AND TEST RESULTS

After the second prototype S-3A Block Assembly (reference 1) was tested at the Naval Air Test Center several problems were uncovered (reference 2);

- a. The method for stowing the assembly in the aircraft aisle was not adequate.
- b. Steel blocks could possibly interfere with the aircraft Magnetic Anomaly Detector (MAD) system.

A third prototype Block was designed and fabricated using aluminum. It also was taken to the Naval Air Test Center for fit and function tests. In addition, static loads were placed on the assembly to determine if the seat restraint straps and the aisle restraint plates were adequate for 10 G crash, catapult, arrestment, and flight loads.

The final configuration of the Ballast Block is shown on the drawings (figures 21 through 28). It differs from the tested assembly as follows;

- a. The final design does not incorporate a rear finger ledge on each block because the crewmen did not use it during evaluation: this ledge was machined into the test blocks.
 - b. The final 1 block is 14.12 inches long in order to completely span the Avionics Bay step; the test 1 block was 13.0 inches long.

These changes will improve the performance of the assembly by increasing its weight, and shifting the center of gravity a bit closer to the rocket thrustline.

CENTER OF GRAVITY TEST (figure 4)

Through a series of ESCAPAC seat suspension tests and mathematical calculations the eccentricity of the 1E1-1 seat/ballast block center of gravity was determined to lie 0.72 inches (1.8 cm) below the rocket thrustline (figure 29). Since the STAPAC rocket is capable of maintaining pitch stabilization of the seat up to an eccentricity of 2.0 inches (5.1 cm) the seat should be adequately stabilized.

The 1E1 ejection seat was designed so that the MK16 rocket thrustline lies about one inch below the seat/50 percentile-man center of gravity. During catapult acceleration the overall center of gravity will shift close to the rocket thrustline to minimize the torque rotating the seat. It is expected that the Ballast Block Assembly will not shift more than 1/8 inch (0.3 cm) downward during the catapult acceleration, and therefore the seat/block center of gravity will shift about half of this amount.

Pitch stabilization is further enhanced due to the lower moment of inertia of the seat/block compared to that of a seat/human, therefore the STAPAC rocket will have greater control on the seat at lower air speeds. At high airspeeds the aerodynamic forces control the seat trajectory more than the rocket force.

CENTER OF GRAVITY OF 1E-1 SEAT WITH S-3A BALLAST BLOCK

TEST CONDITIONS:

- 1. Ballast Block assembly tested without fore and aft extensions on bottom block.
- 2. IG-2 ESCAPAC seat used with parachute, empty RSSK, and empty catapult.
- 3. All measurements made from lower seat roller; Z along roller centerline.

DATA:

Weight of Ballast Block W_R = 164.0 pounds

Weight of IG-2 seat $W_{IG-2} = 108.3$

Weight of 1E1-1 seat complete (empty) W_{1F1} = 146.9

C.G. of IG-2 seat with Block (12.9, 14.7) inches

C.G. of IG-2 seat empty (7.9, 17.2)

C.G. of 1E-1 seat complete (empty) (7.9, 15.0)

MK 16 Rocket thrustline intercepts roller centerline 6.8 inches above bottom roller; 57 degrees from roller centerline

CALCULATIONS:

1 LOCATION OF BLOCK C.G. RELATIVE TO BOTTOM ROLLER OF IG-2 SEAT

 $W_{IG-2} \cdot x_{IG-2} + W_B \cdot X_B = W_{IG-2/B} \cdot x_{IG-2/B}$

 $(108.3) 7.9 + 164.0 \times_B = (108.3 + 164.0) 12.9$

 $X_B = 16.2$

 $W_{IG-2} \cdot Z_{IG-2} + W_B \cdot Z_B = W_{IG-2/B} \cdot Z_{IG-2/B}$

 $(108.3) 17.2 + 164.0 Z_B = (108.3 + 164.0) 14.7$

 $Z_B = 13.0$

II LOCATION OF 1E-1 SEAT/BALLAST BLOCK CENTER OF GRAVITY

 $W_{1E-1} \cdot X_{1E-1} + W_B \cdot X_B = W_{1E1-1/B} \cdot X_{1E-1/B}$

 $(146.9) 7.9 + (164.0) 16.2 = (146.9 + 164.0) X_{1E-1/B}$

 $X_{1E-1/B} = 12.3$

 $W_{1E-1} \cdot Z_{1E-1} + W_B \cdot Z_B = W_{1E-1/B} \cdot Z_{1E-1/B}$

 $(146.9) 15.0 + (164.0) 13.0 = (310.9) Z_{1E-1/B}$

 $Z_{1E-1/B} = 13.9$

III ROCKET THRUST ECCENTRICITY WITH 1E-1 SEAT/BLOCK CENTER OF GRAVITY

slope of rocket thrustline

$$m = tan (90^{\circ} - 57^{\circ}) = .649$$

slope of perpendicular to thrustline

$$m_{\perp} = -\frac{1}{M} = -\frac{1}{.649} = -1.54$$

rocket thrustline equation

$$Z = 0.649 \times +6.8$$

line perpendicular to thrustline thru 1E-1/block C.G.

$$Z = -1.54 \times + b$$

 $13.9 = -1.54 (12.3) + b$
 $b = 32.8$

 $Z = -1.54 \times + 32.8$

INTERCEPT OF BOTH LINES (ROCKET THRUST AND PERPENDICULAR)

$$Z = 0.649 \times + 6.8$$

$$Z = 0.649 (11.9) + 6.8$$

$$Z = -1.54 \times + 32.8$$

$$2.19 \times = 32.8 - 6.8$$

$$X = 11.9$$
 inches

C.G. ECCENTRICITY

$$e = [(Z_2 - Z_1)^2 + (X_2 - X_1)^2]^{1/2}$$

$$e = [(14.5 - 13.9)^2 + (11.9 - 12.3)^2]^{1/2}$$

e = 0.72 inches below thrustline

ASSEMBLY AND DISASSEMBLY ON THE 1E-1 SEAT AND ON THE AISLE STEP

Two blocks at a time can be carried to the aircraft by one crewmember (figure 3).

The first block (-1 Block) should be placed on the RSSK-8A survival kit so that the aft tabs rest against the survival kit back fittings (figure 8). After the other three blocks are stacked onto the seat (figure 9) the shoulder restraint straps are routed up through the block handles and connected to the parachute risers (figures 10,11). Then the 'lap belt' on the top block is connected to the survival kit straps (figures 12, 13). All straps are then tightened, and the inertia reel lever is placed in the 'lock' position.

When the Assembly is to be stowed on the avionics aisle step the -1 Block is placed with the handle towards the aircrafts' port side, and the block tangs slide under the lip of the step bulkhead (figure 14). The other three blocks are then stacked on top (figures 15, 16, 17), then the top locking plates are slid into the bulkhead forgings and secured by the two wing nuts (figures 18, 19, 20).

EJECTION SEAT STATIC LOADS

The existing seat lap belt/shoulder harness straps are used to restrain the Ballast Block Assembly. Since these straps are qualified for crash loads it was decided that one test would be sufficient to verify structural integrity of the assembly on the seat.

<u>Forward</u> — A forward load of 1000 pounds was applied to the block assembly simulating a —6 Gx arrested landing; no problems were encountered (figure 5).

Aft — When subjected to catapult loads the Block Assembly is prevented from moving aft by the lap belt strap and seat back. No test was conducted.

<u>Vertical</u> — For vertical loads the Assembly is restrained by the lap belt and seat bucket which are capable of handling all Gz flight or crash design loads on the aircrewman. No test was conducted.

<u>Lateral</u> — Lateral stability is assured by the bottom block side tabs (figure 8) which limit the block center of gravity movement to about 1/2 inch (1.3 cm); this translates to less than 1/4 inch (0.6 cm) of seat/block center of gravity movement. No test was conducted.

AISLE POSITION STATIC LOADS

Aft (Catapult) Loads (figure 6) — A ratchet winch was used to place a 1000 pound aft load on the block assembly to simulate a +6 Gx catapult launch. No problems were encountered.

Forward (Arrestment) Loads — No test was conducted because the Block Assembly contacts the lower section of the avionics bay bulkhead. The entire center aircraft structure would have to fail before the Block Assembly could break loose.

Upward (-Gz) Flight Loads (figure 7) - A ratchet winch was used to place a 500 pound upward load on the Assembly to simulate a -2Gz flight load. This exceeds the design flight loads of the aircraft. No problems were encountered.

Side (\pm Gy) Loads (figure 20) — The aisle locking plates limit the lateral motion of the top block to \pm 1/4 inch (1 centimeter). The bottom block is limited to the same motion before contacting the sides of the aisle. No tests were necessary.

<u>Downward (+Gz) Crash Loads</u> — There is a requirement that all new equipment installed in the aircraft must be capable of withstanding a crash load of 10G without breaking loose from its support points. Since the bottom block of the assembly completely spans the avionics bay step the foam core aluminum step has no bending loads. All the load can easily be taken into the angles which support the step (figure (14). Even if the step should fail the Block Assembly would be limited in its vertical motion because of the electronic equipment directly beneath the step. No actual test was conducted.

CONCLUSIONS

- 1. The S-3A Ballast Block meets all operational and structural requirements for safe utilization in the aircraft.
- 2. The Ballast Block provides a simple and cost effective replacement for the anthropomorphic dummies presently being used to ballast unoccupied 1E-1 ejection seats.

ACKNOWLEDGEMENTS

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- 1. Lorch, Dan, 4 Nov 1981, Development of An Ejection Seat Ballast Block for the S-3A Aircraft, Report No. NADC-81272-60 Naval Air Development Center, Warminster, PA 18974.
- 2. Stark, G/Sparks, T., AME 1, July 1981 Feasibility Evaluation of Proposed S-3A Aircraft Ejection Seat Ballast Block Report No. SY-62R-82 Naval Air Test Center, Patuxent River, MD 20670.



Figure 1. S-3A Ballast Block Assembled

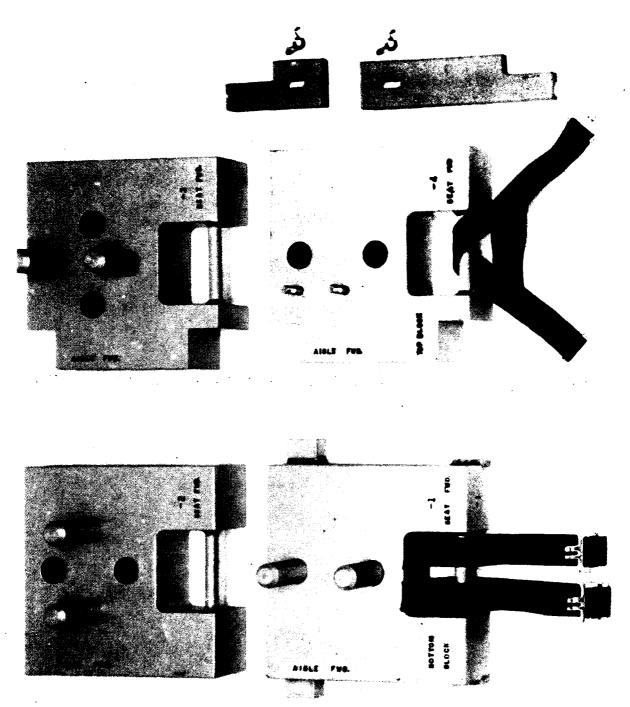


Figure 2. S-3A Ballast Block Disassembled

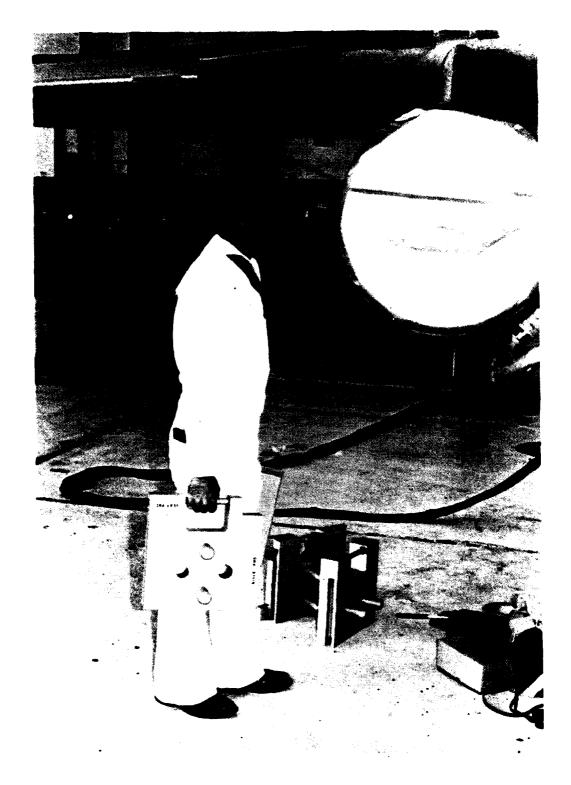


Figure 3. Crewman Carrying Ballast Block Components

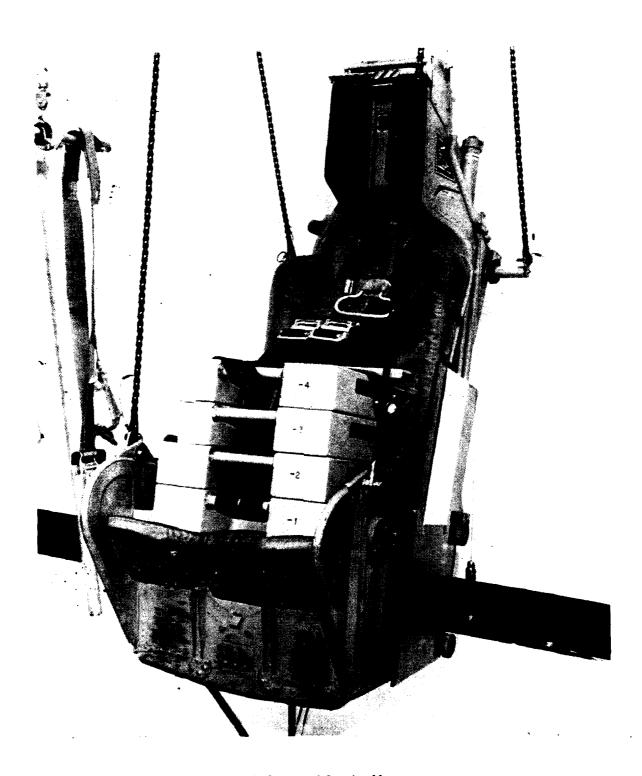


Figure 4. Center of Gravity Measurement



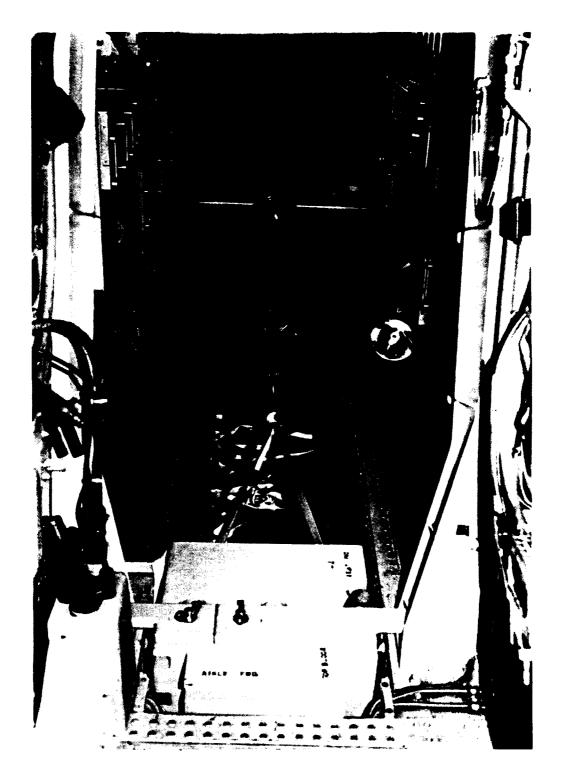


Figure 6. 1000 Pound $+G_X$ Load in Aisle



Figure 7. 500 Pound $-G_z$ Load in Aisle

Figure 8. -1 Bottom Block in Seat



Figure 9. -2 Block Placed in Seat

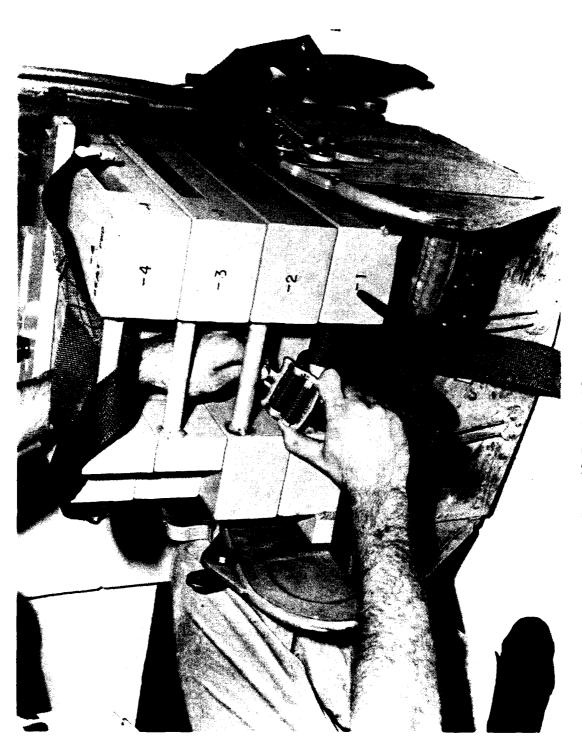


Figure 10. Routing of Shoulder Restraint Straps

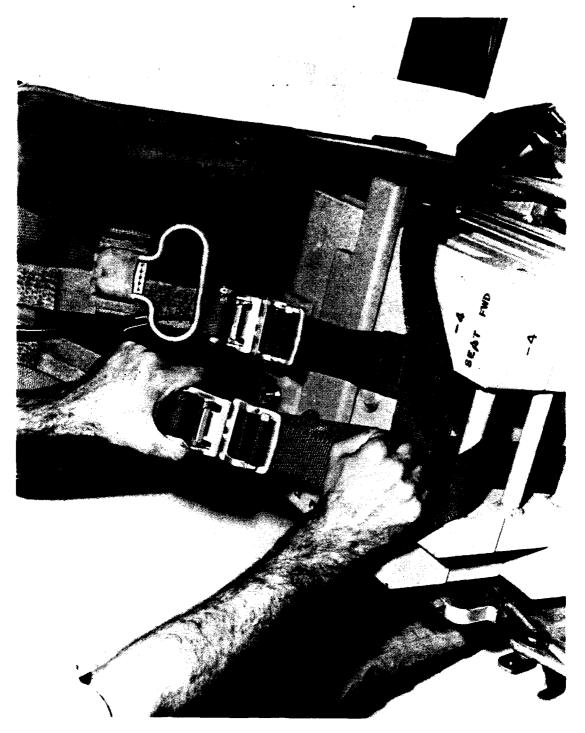


Figure 11. Connecting Parachute Riser Straps



Figure 12. Connecting Lap Belt Fittings

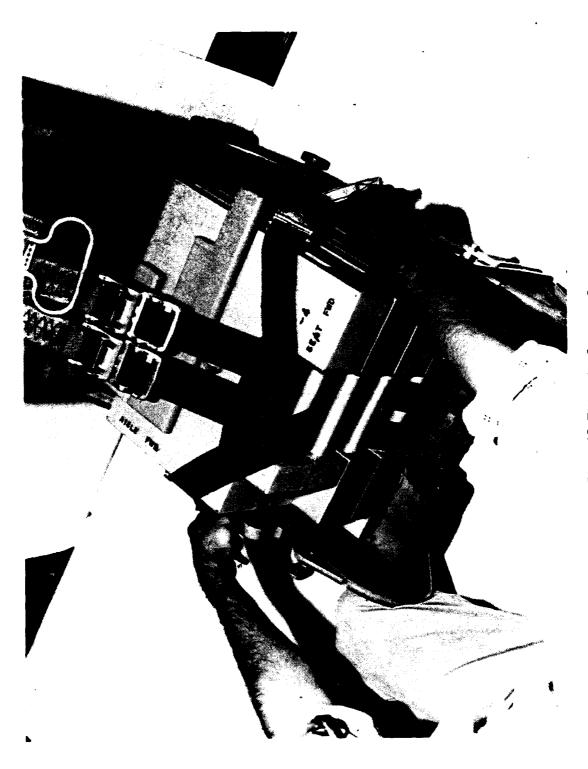


Figure 13. Tightening Straps on Seat

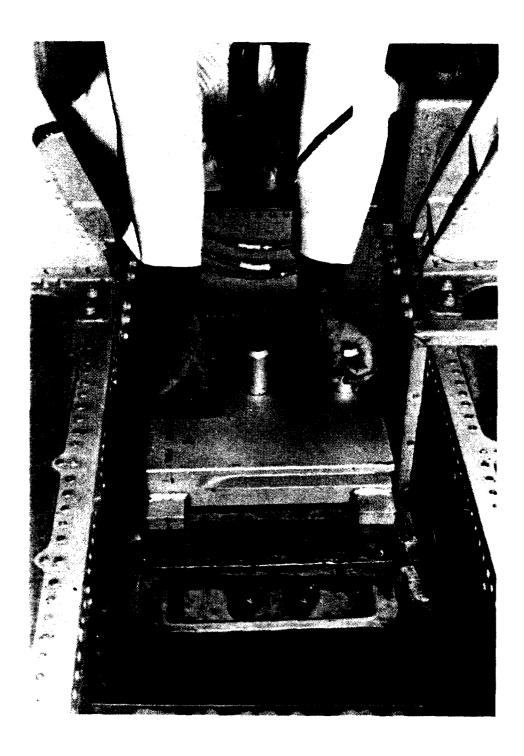


Figure 14. -1 Block on Aisle Step



Figure 15. -2 Block on Aisle Step



Figure 16. -3 Block on Aisle Step



Figure 17. —4 Block on Aisle Step

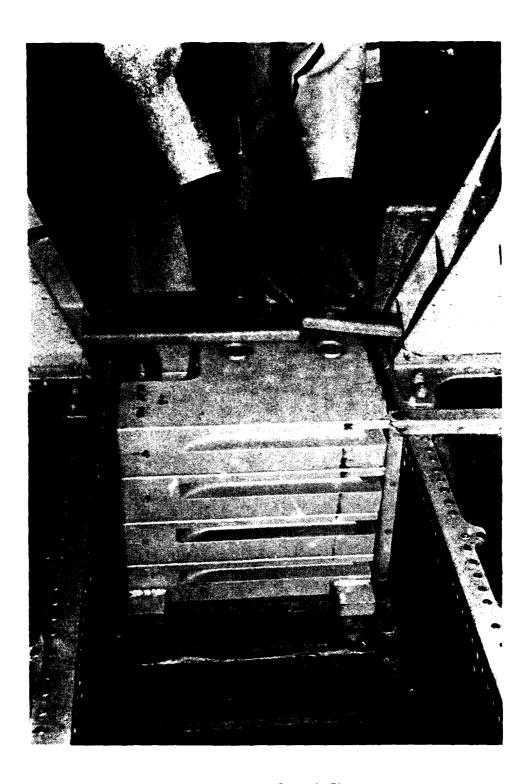


Figure 18. Lock Plates in Place

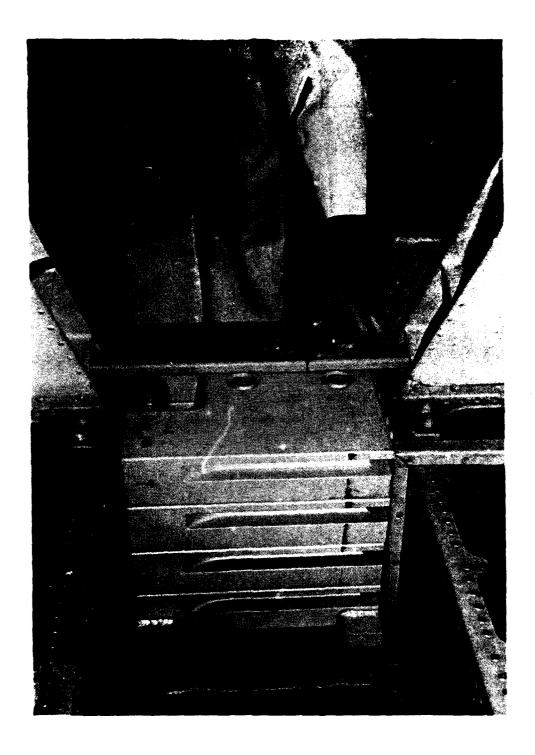
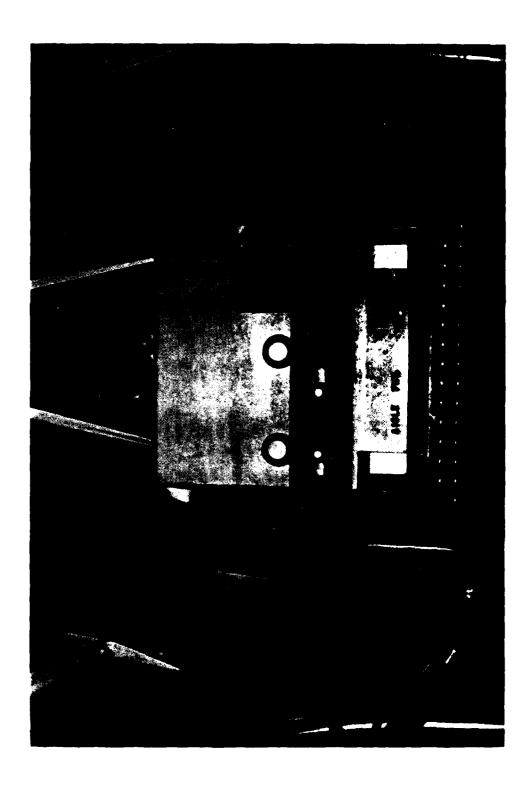
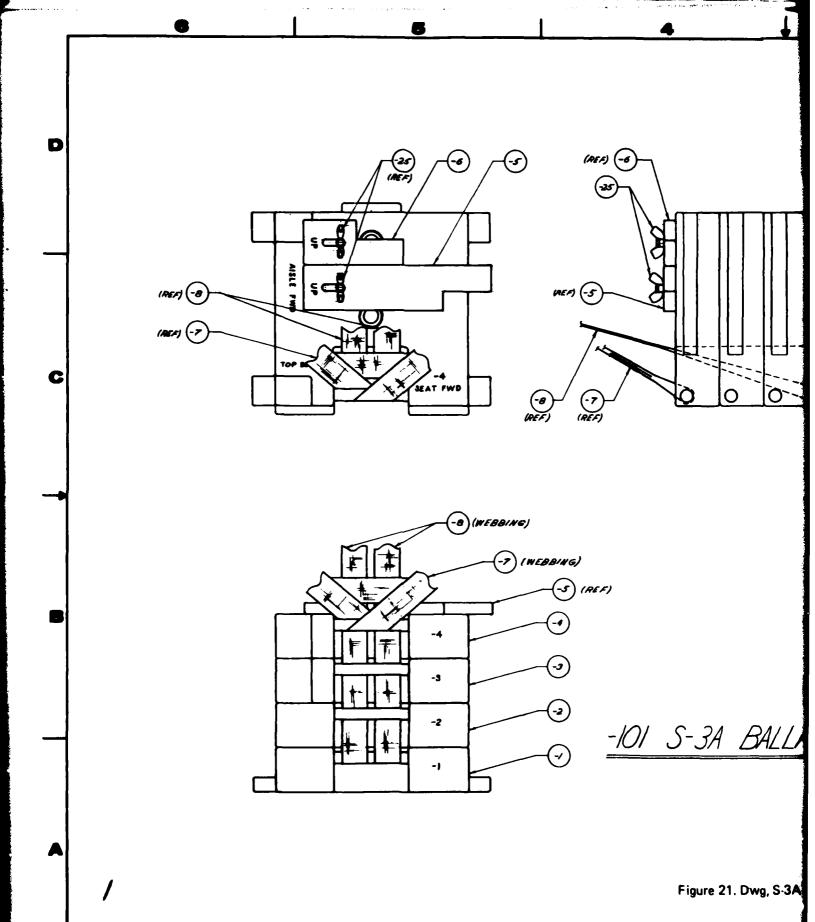
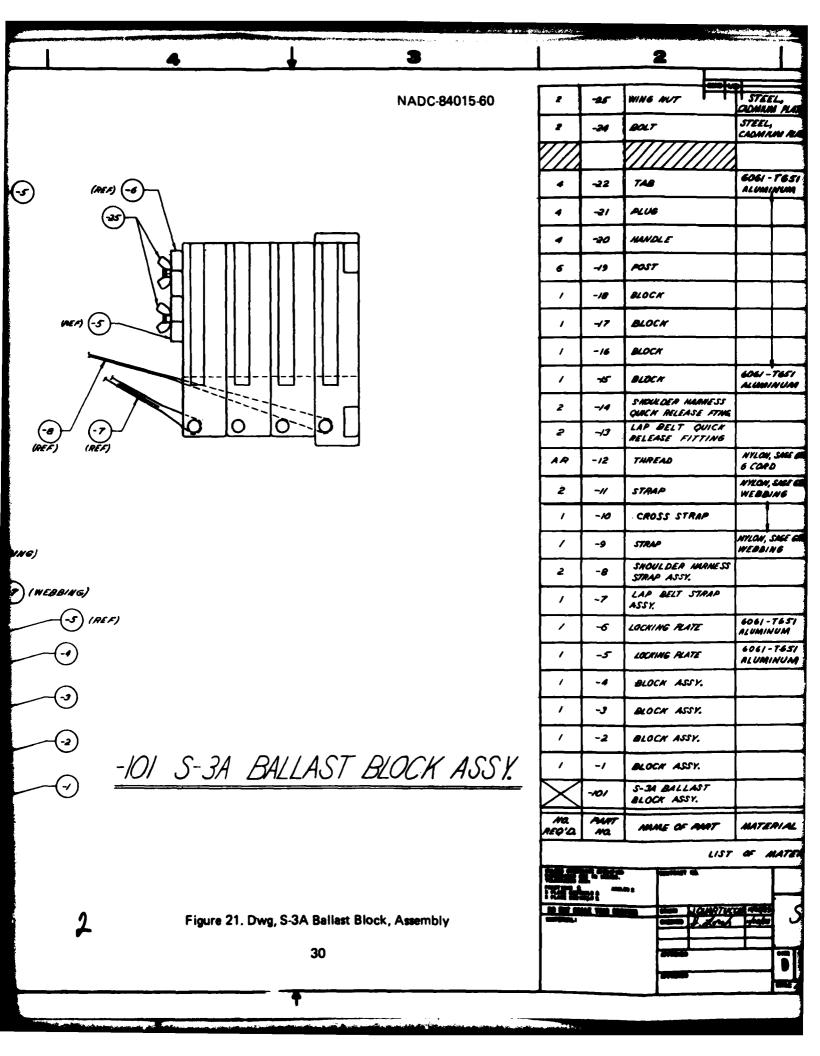
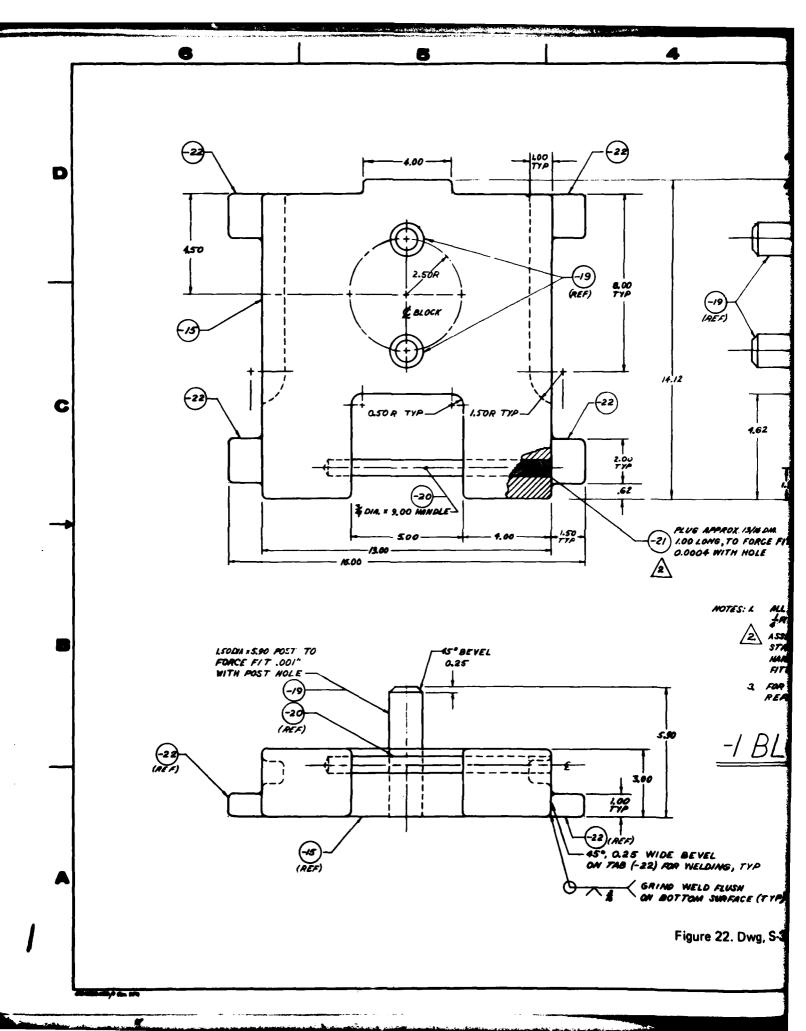


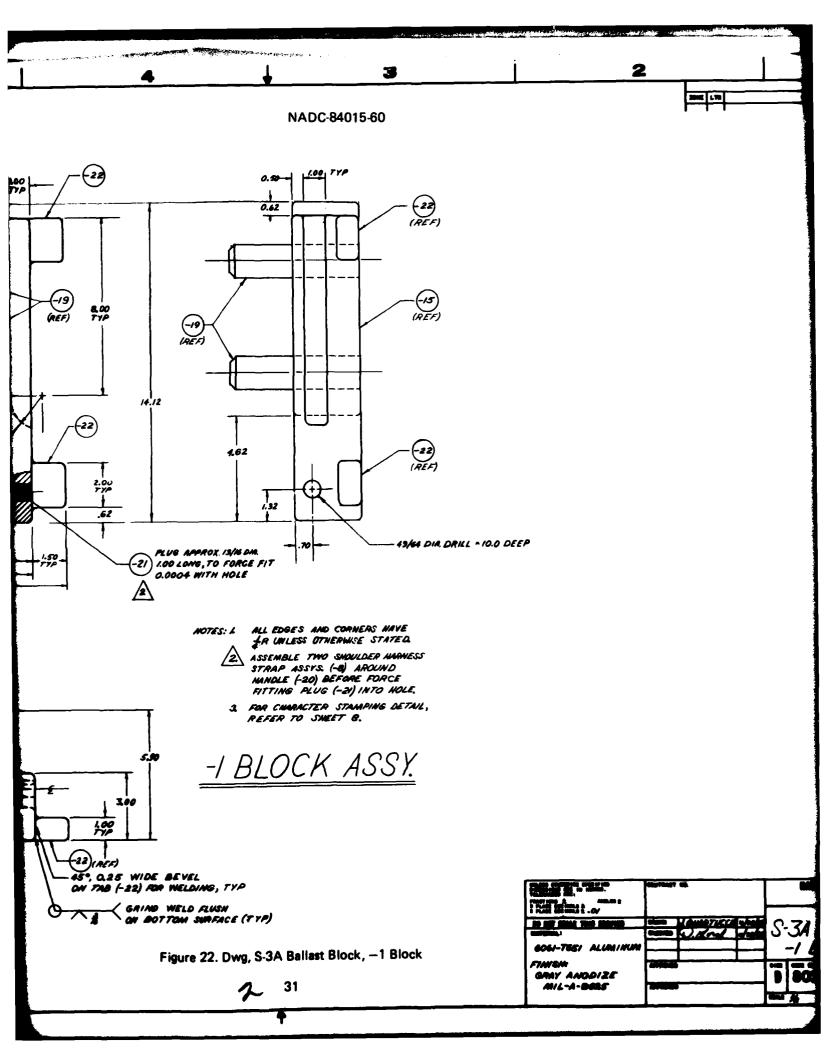
Figure 19. Wing Nuts on Locking Plates

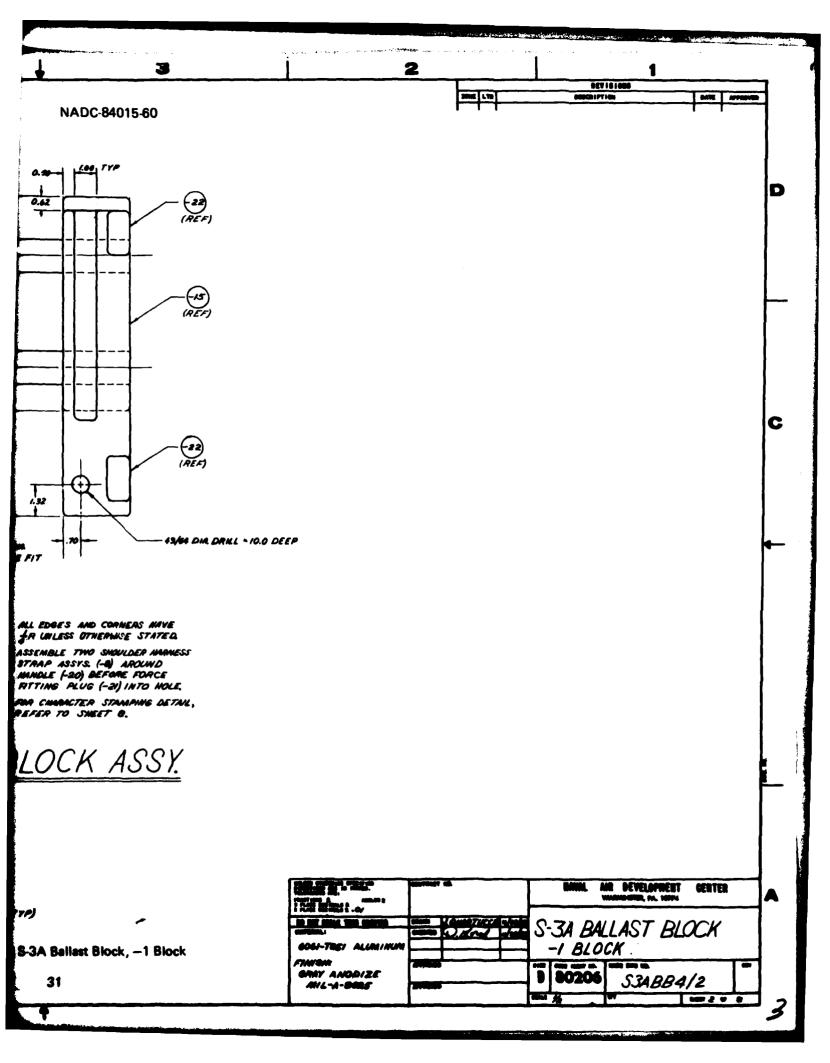


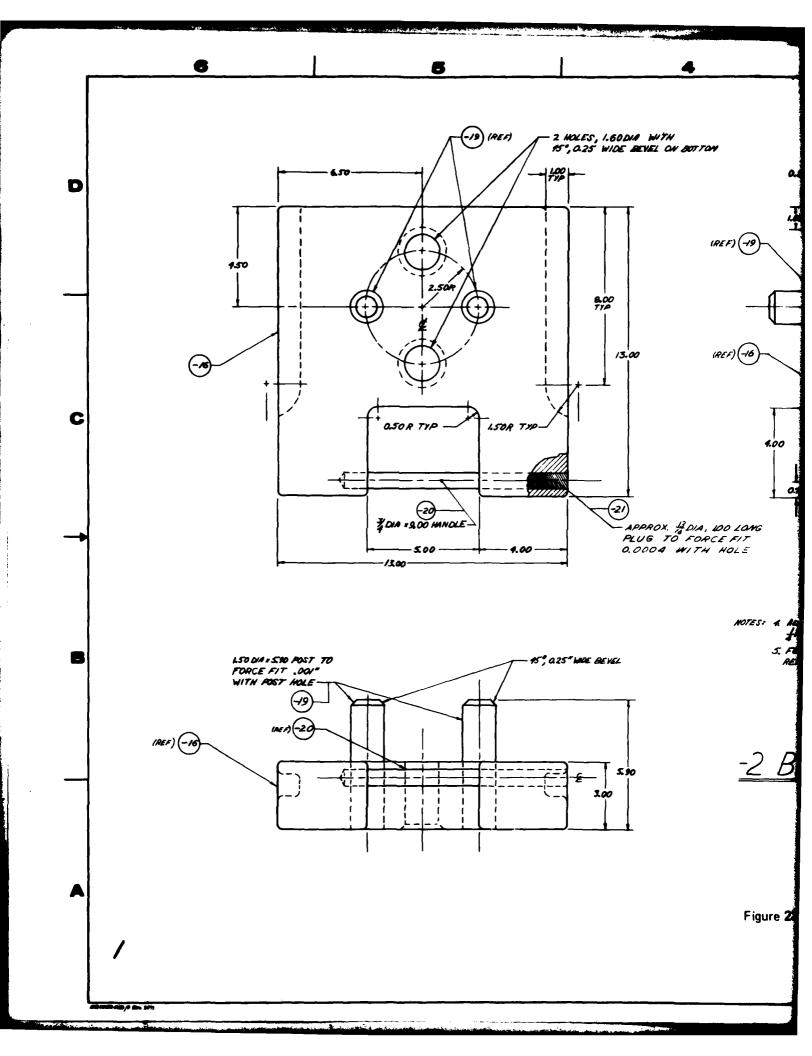






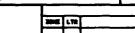


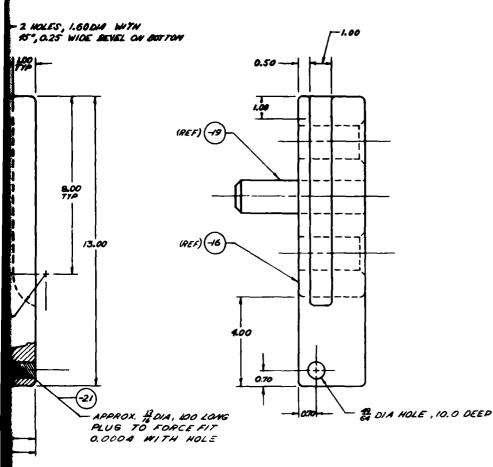






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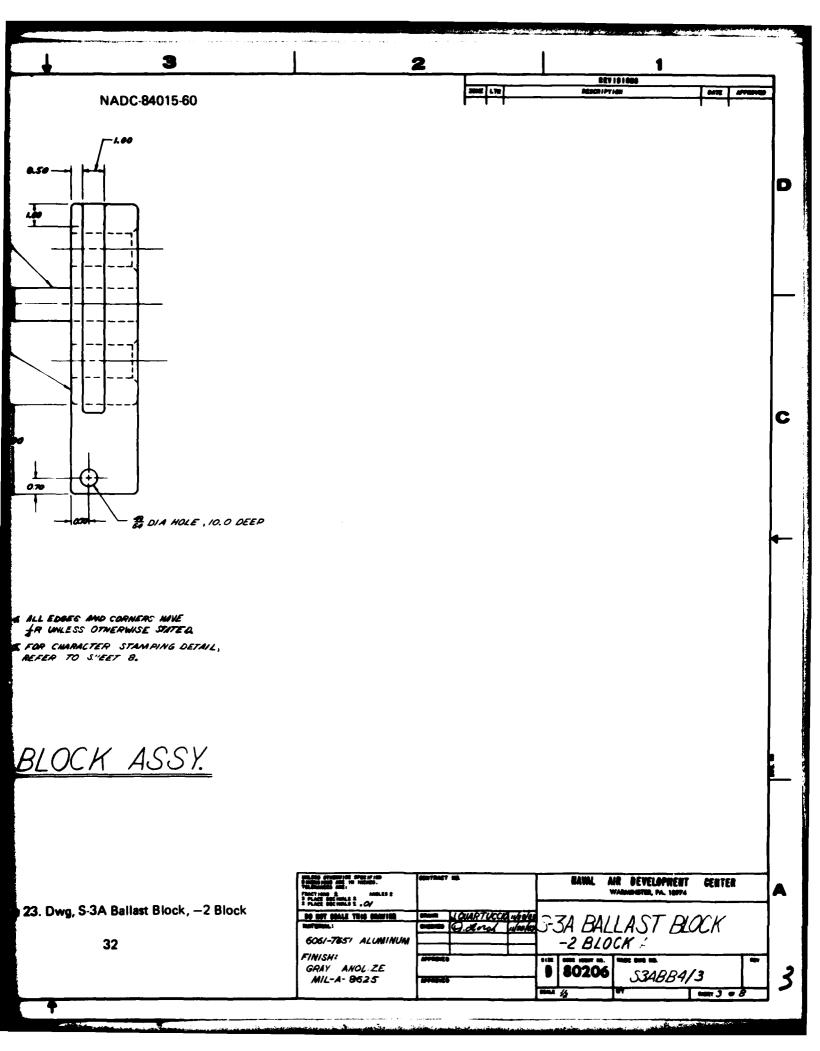
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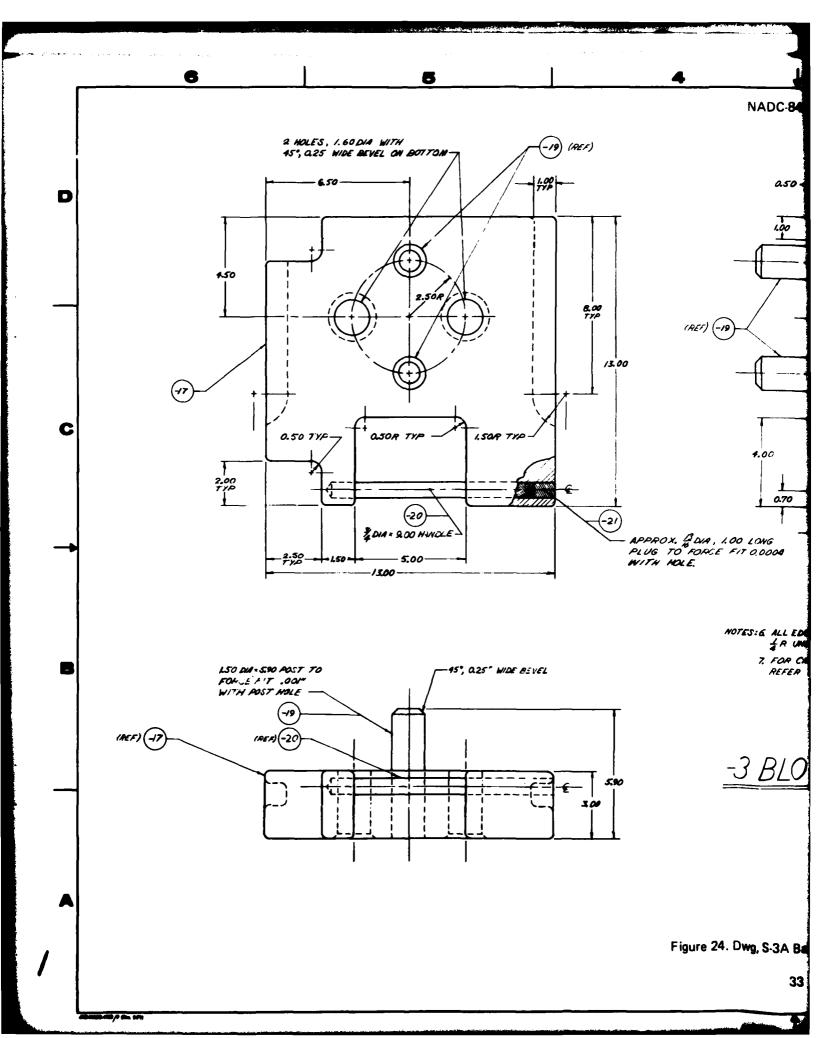
Figure 23. Dwg, S-3A Ballast Block, -2 Block

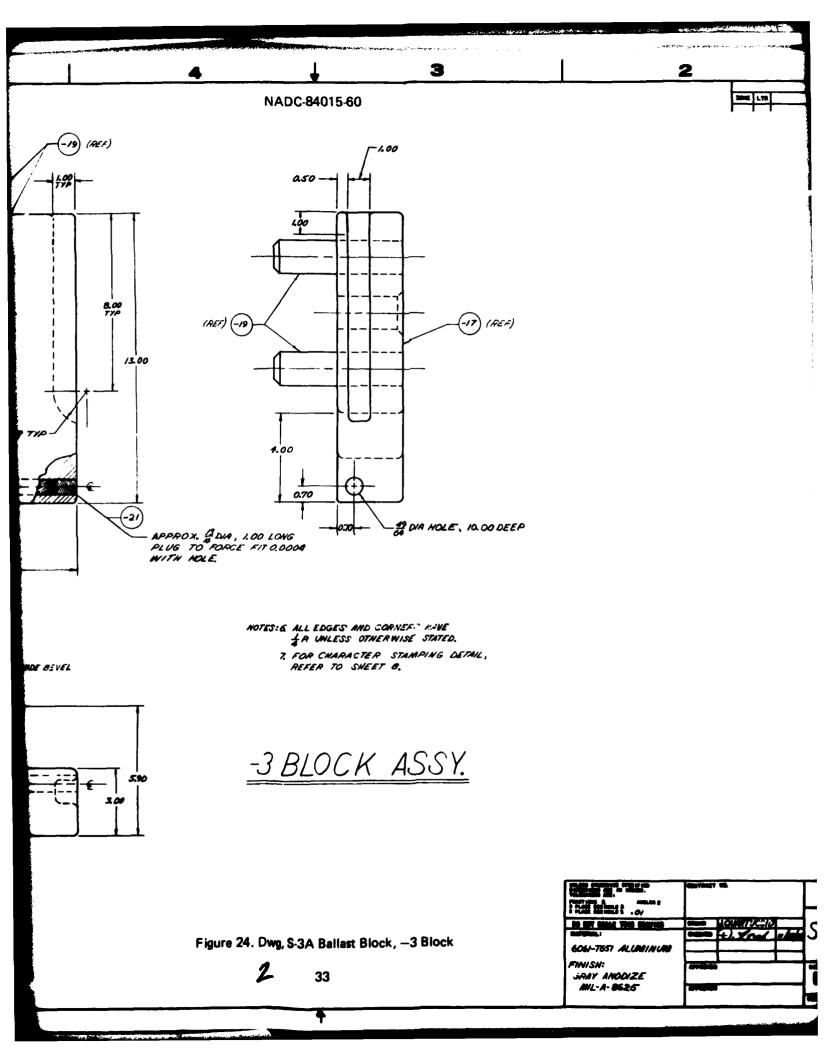
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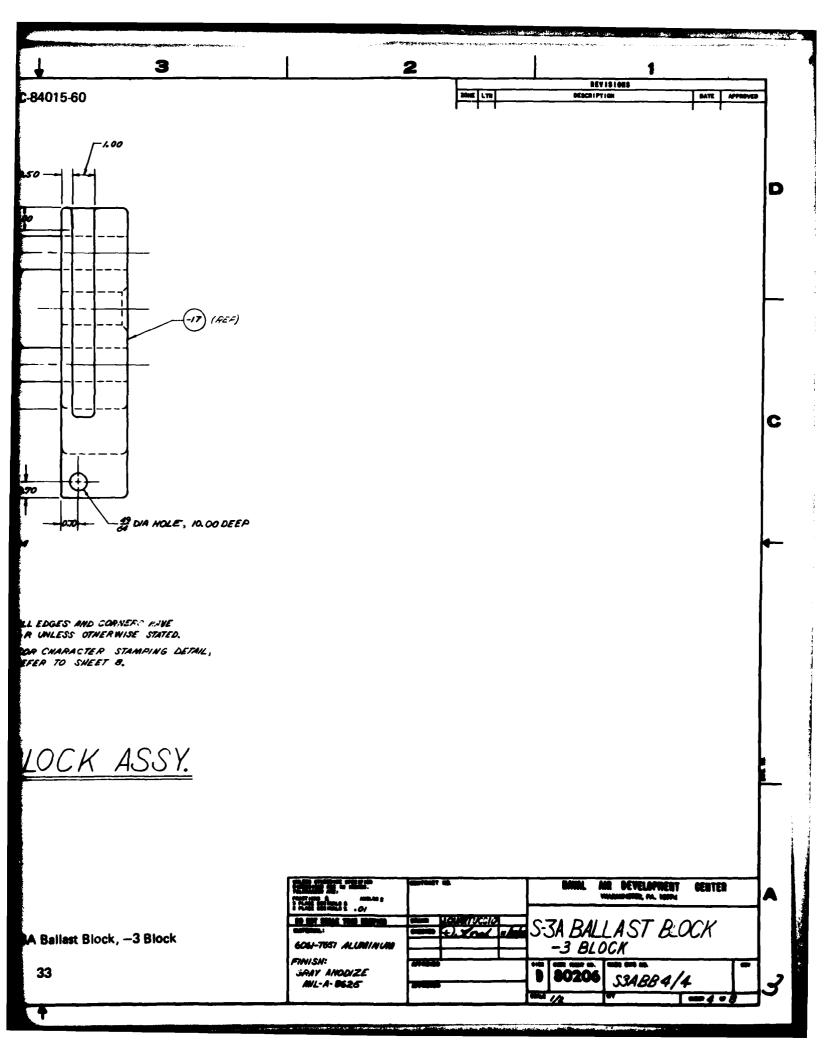
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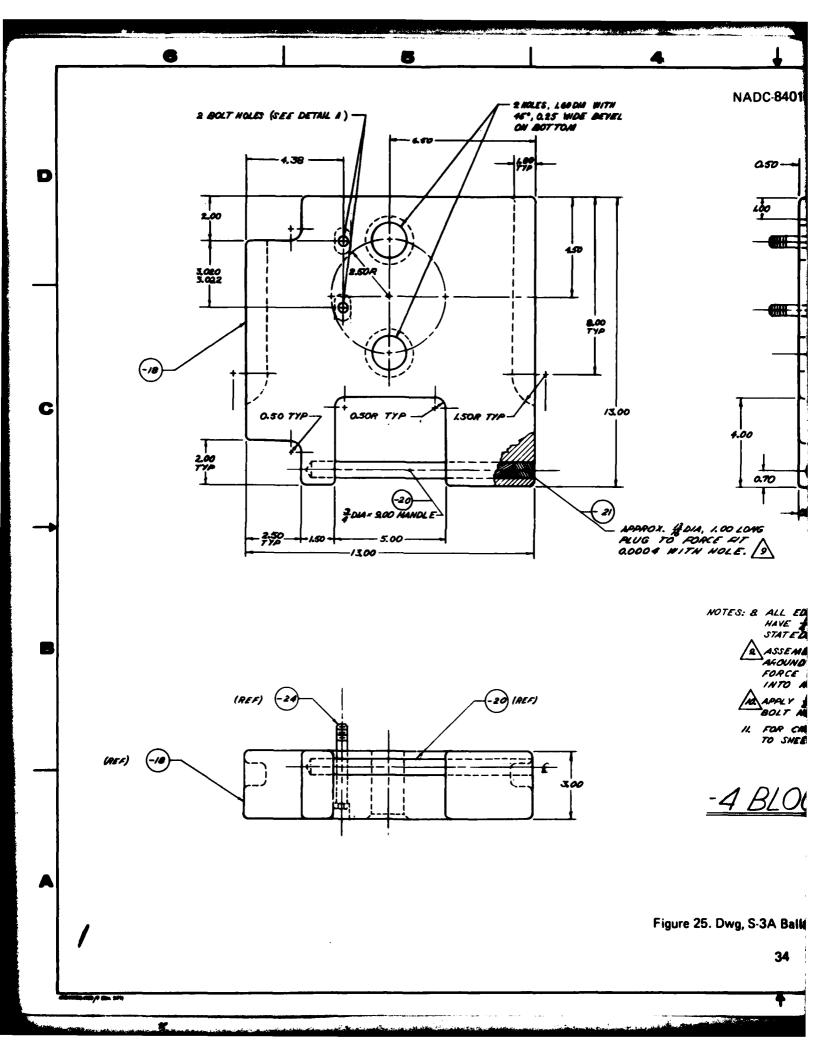
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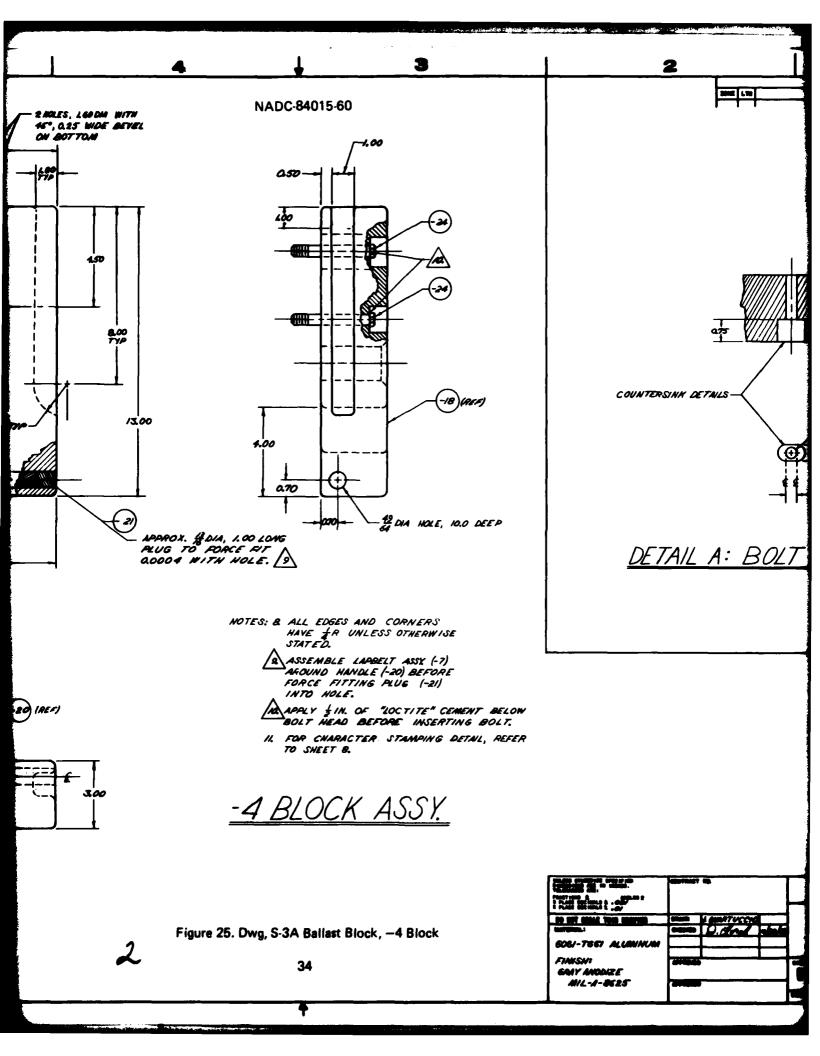


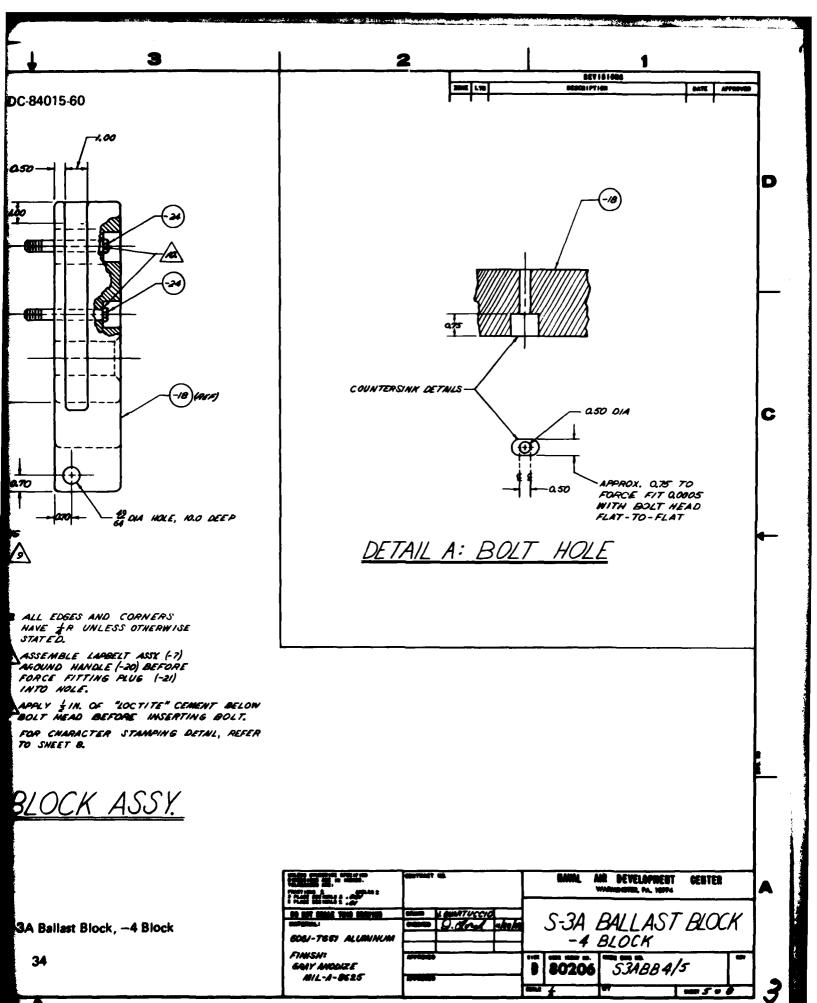




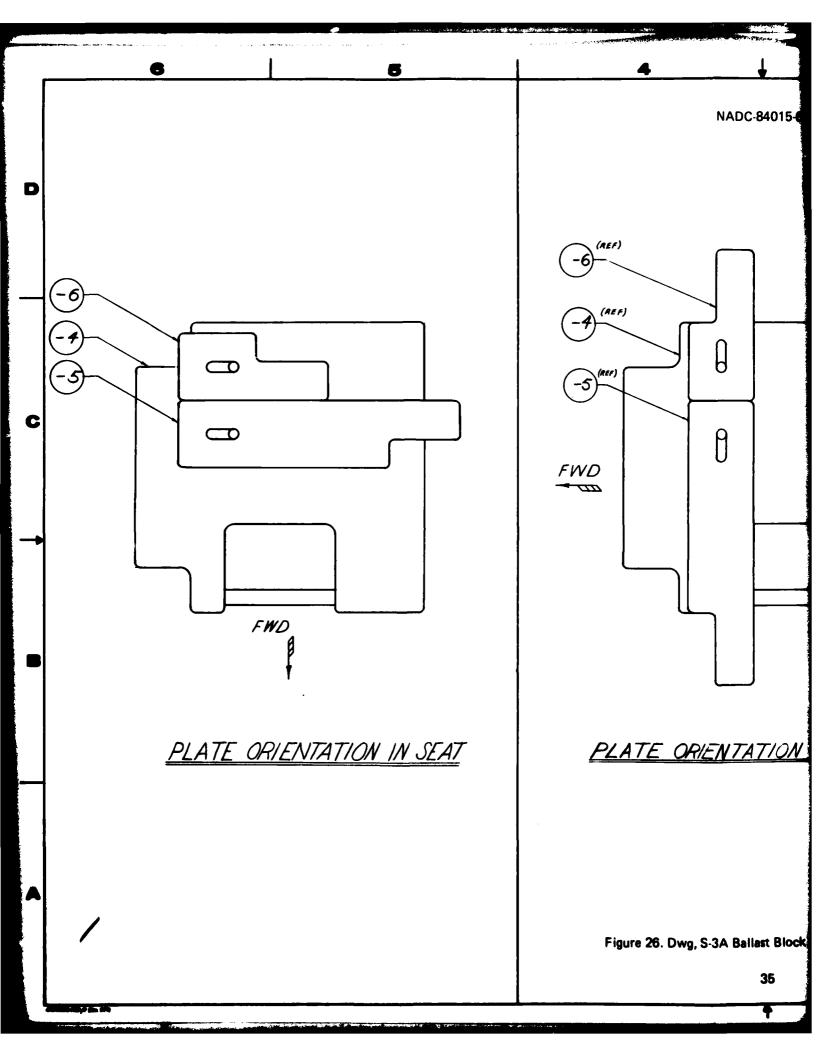


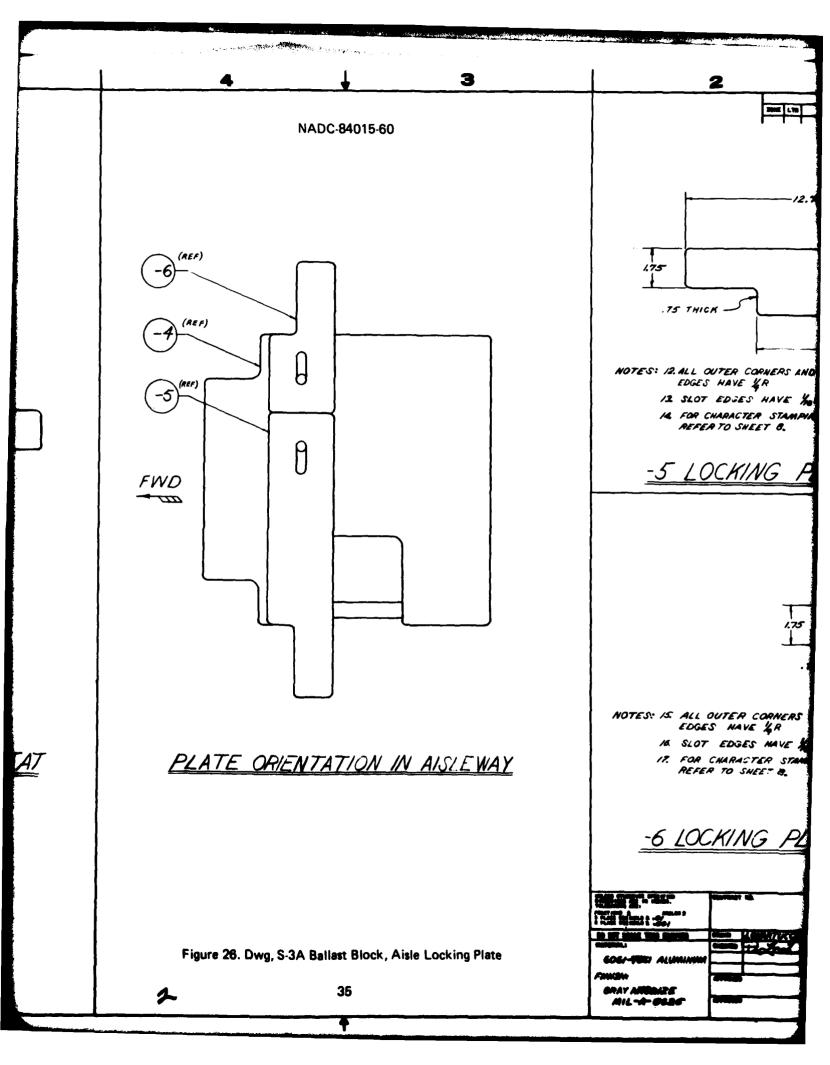


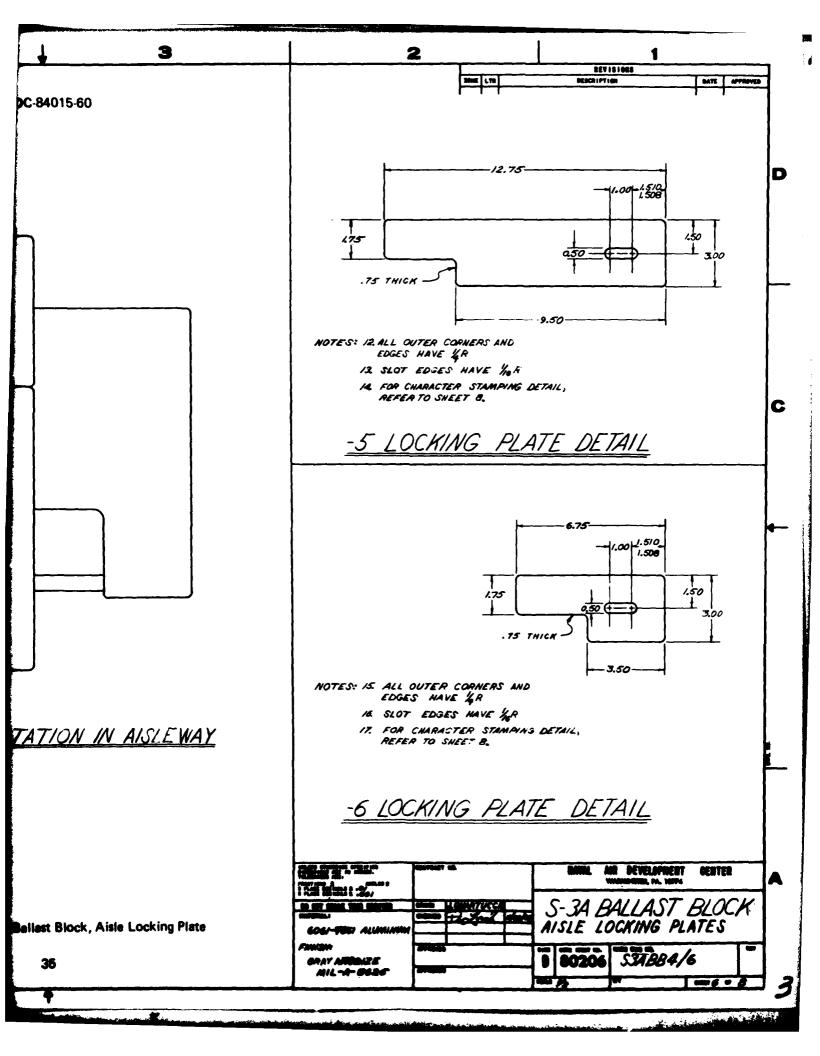




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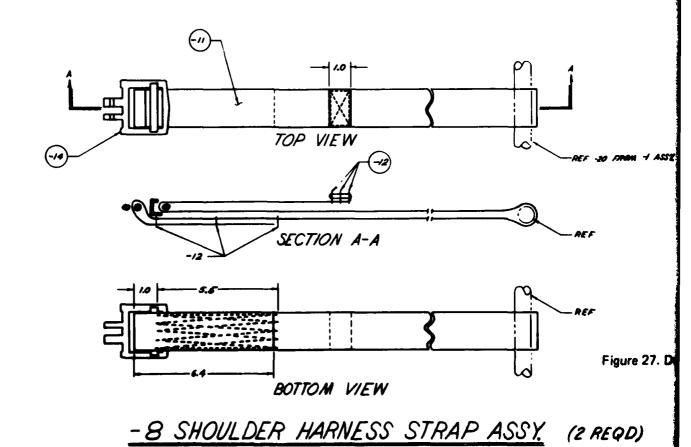
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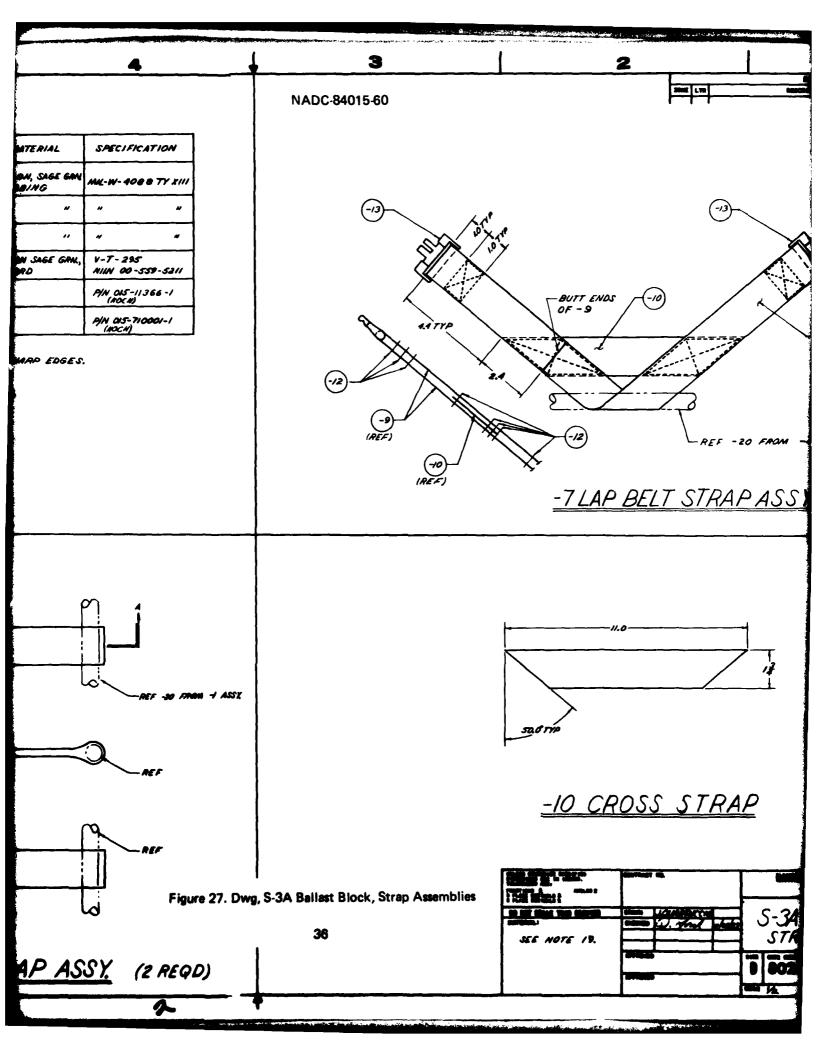
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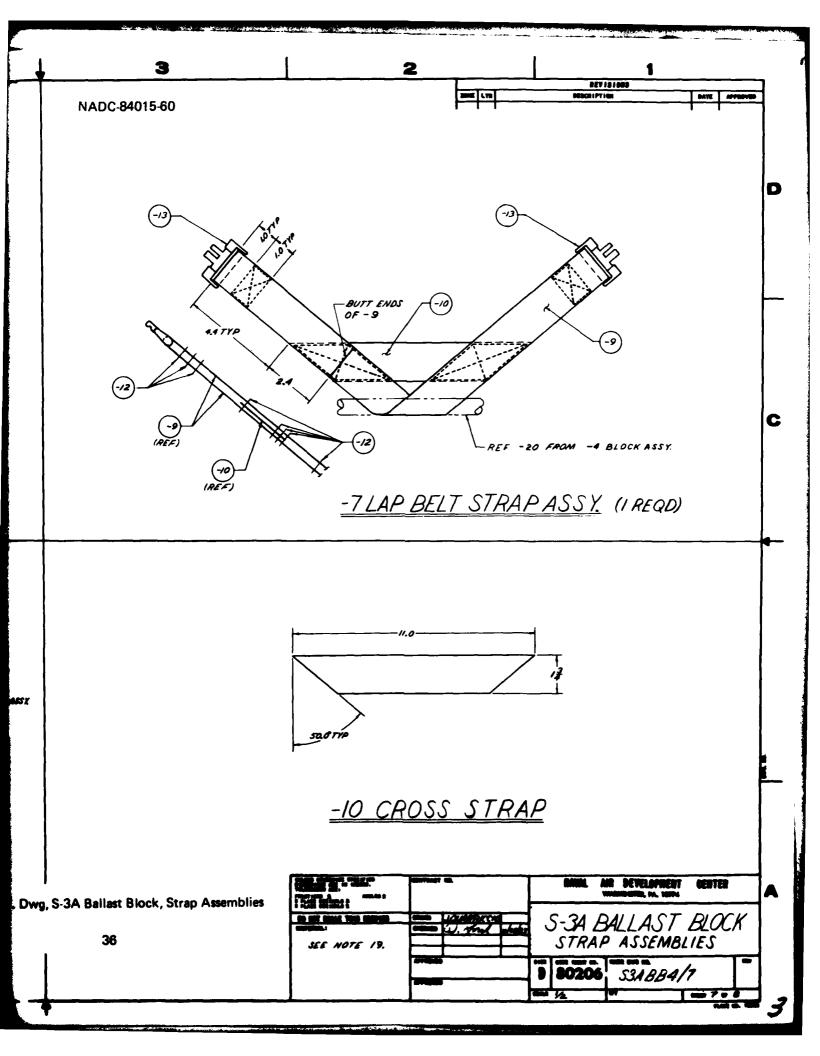
A MATERIALS (REFERTED FROM SHEET 1):

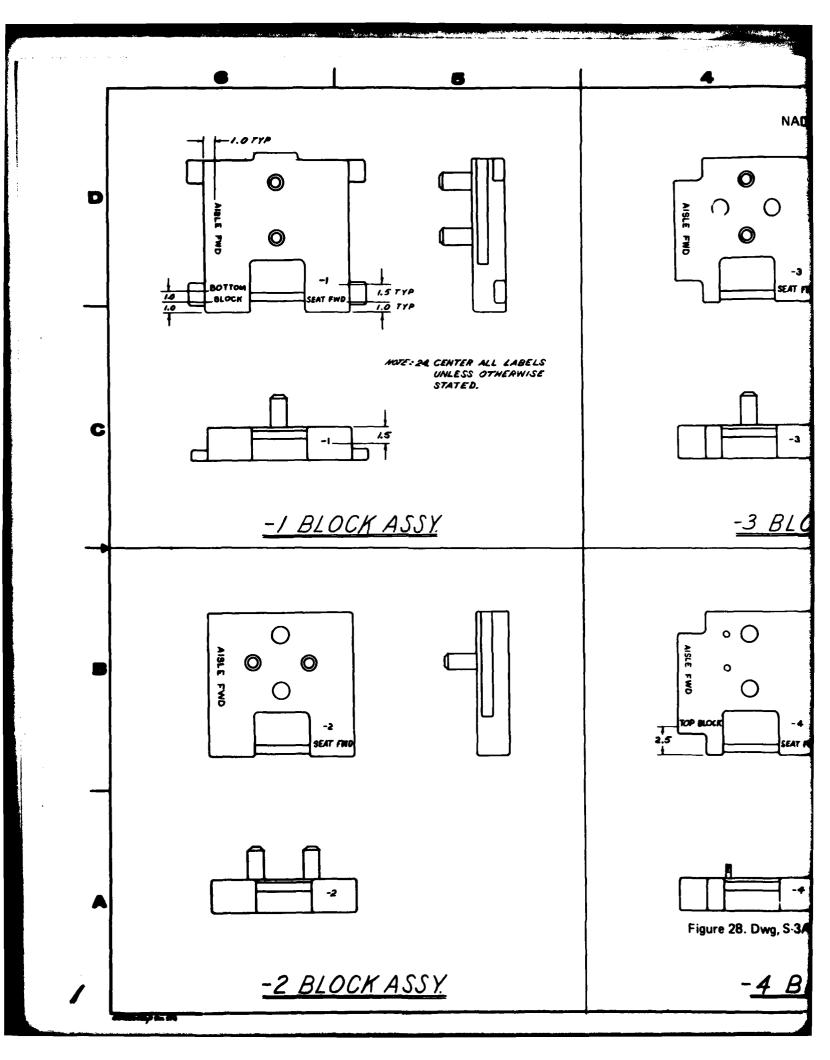
PART NO.	MO, MEGO MEM ASS X	DESCRIPTION	S/ZE	MATERIAL	SPECIFICATION
-9	,	LAP BELT STRAP - ONE CONTINUOUS STRAP, LOOPED BACK ON ITSELF	13 + 44	NYLON, SAGE GAN WEBBING	ML-W-4088 TY XIII
-10	/	CAOSS STRAP	13-11	" "	" "
-//	2	SHOULDER MARNESS STRAP	13 = 54	" "	,, N
-12	AS MEQUARED	THREAD		NYLON SAGE GAM, 6 COAD	V-T-295 NIIN 00-559-5211
-/3	2	LAP BELT QUICK RELEASE FITTING			P/N 015-11366-1 (NOCN)
-/4	2	SHOULDER MARNESS QUICN RELEASE FITTING			P/N 015-710001-1 (NOCH)

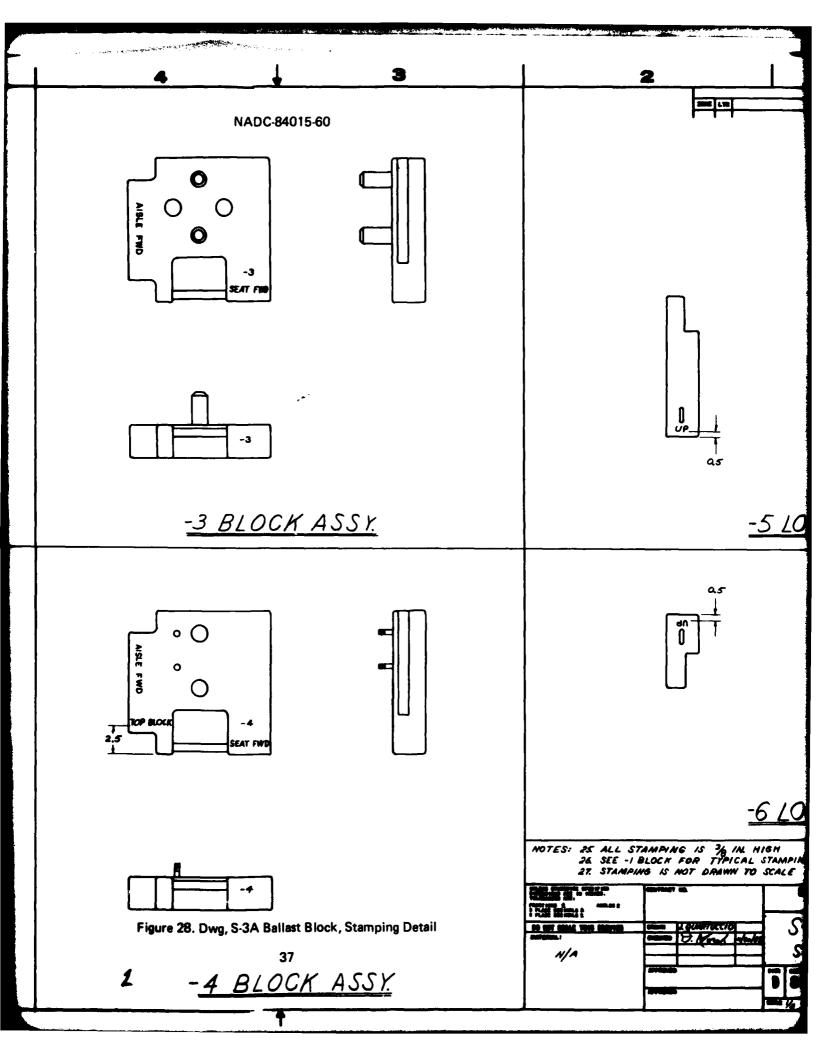
20 SEAR ENDS OF NYLON WEBBING TO PREVENT FRAYING, AVOID FORMING SHARP EDGES.
21 ALL STITCHING SHALL BE 4 TO 6 THREADS PER INCM.
22 STITCHING ALONG EDGE SHALL BE \$IM. AWAY FROM EDGE OF WEBBING.
23 ALL STITCHING SHALL BE BACKSTITCH \$ MIN.

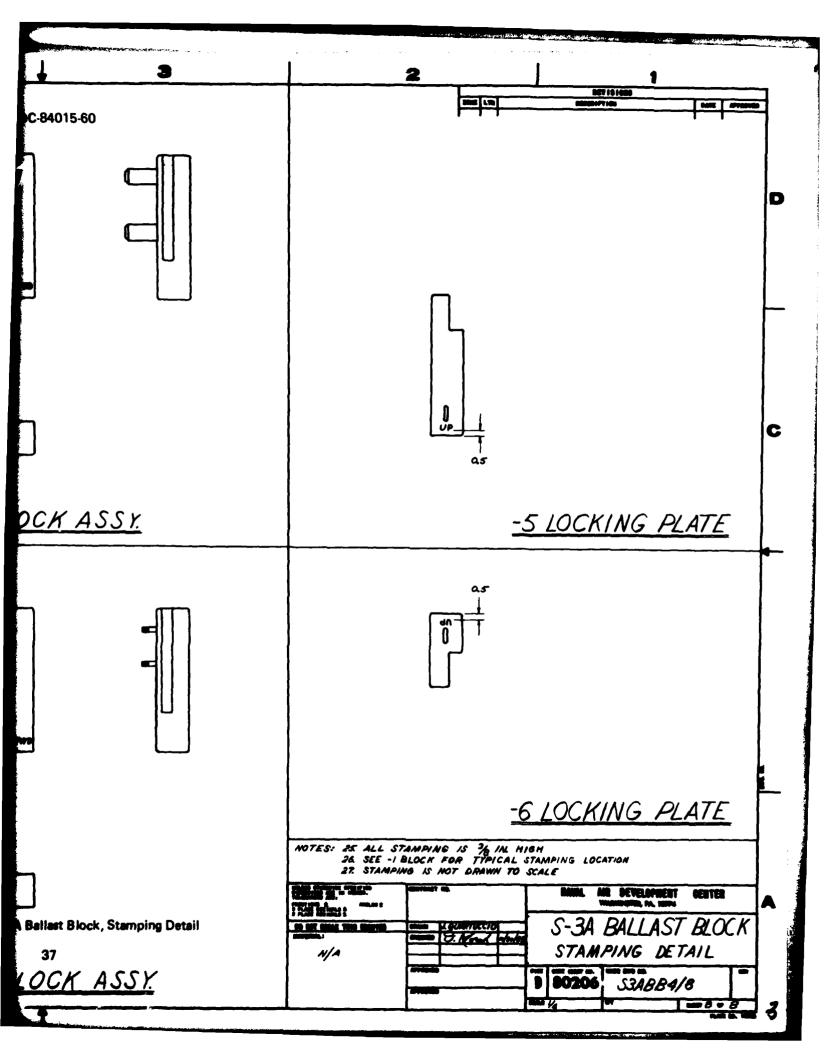












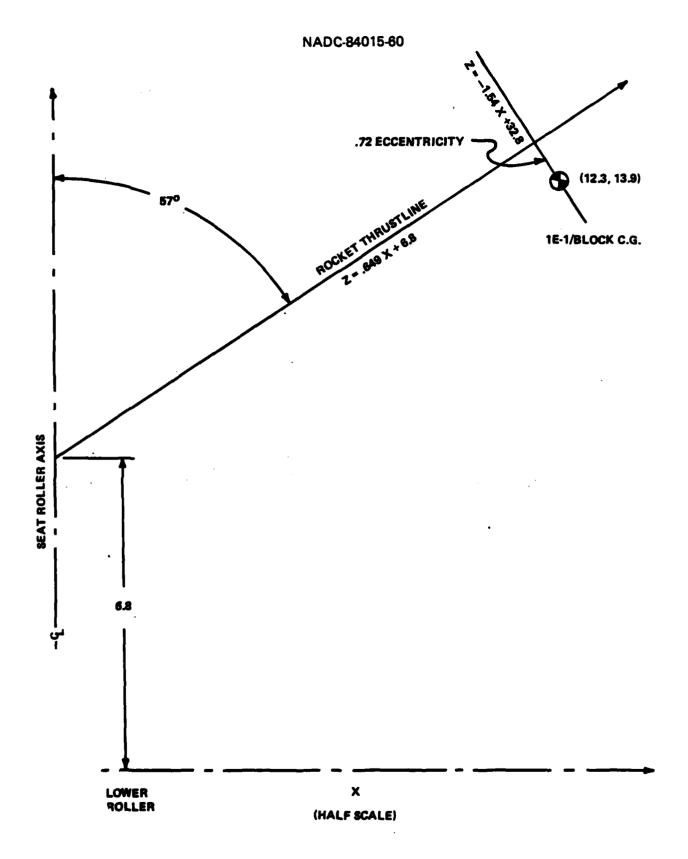


Figure 29. 1E-1 Ballast Block C.G. Eccentricity with Rocket Thrustline